



STDC Soil Treatment Hospital, Redcar, Teesside

Flood Risk Assessment & Drainage Strategy South Tees Development Corporation

12 May 2021

Notice

This document and its contents have been prepared and are intended solely for South Tees Development Corporation's information and use in relation to a detailed planning application for a proposed temporary soil treatment hospital at the Former Redcar Steelworks site in Redcar, Teesside.

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Document history

Revision	Purpose description	Originated	Checked	Reviewed	Authorised	Date
1.0	First issue	FL	PJB	IK	IK	12/05/2021



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1. Introduction

Atkins has been commissioned by South Tees Development Corporation to prepare a Flood Risk Assessment and Drainage Strategy to support a detailed planning application for a proposed temporary soil treatment hospital (the "Proposed Development"), lasting approximately five years, on a parcel of land at the Former Redcar Steelworks, Redcar, Teesside (the "Site").

This Flood Risk Assessment has been prepared in accordance with the National Planning Policy Framework (NPPF)¹ and associated Planning Practice Guidance². The scope of this Assessment has been established through consultations with the Environment Agency, the Lead Local Flood Authority (LLFA) (Redcar & Cleveland Borough Council) and Northumbrian Water Ltd.

¹ National Planning Policy Framework, June 2019, Department for Communities & Local Government.

² Planning Practice Guidance, October 2019, Department for Communities & Local Government.



2. Background Information

2.1. Environment Agency (EA)

An enquiry was submitted to the Environment Agency. The response received is summarised below and included in full in **Appendix A**:

- The Site is within Flood Zone 1. The EA have no record of flooding in the area. This does not necessarily mean that the site has never flooded, only that the EA do not currently have records of flooding in this area.
- The EA advise contacting the LLFA in relation to drainage discharge rates, local flood risk from ordinary watercourses, surface water and ground water flooding. The EA recommend contacting Northumbrian Water Ltd regarding flood risk from sewers.

2.2. Northumbrian Water Ltd

A Developer Enquiry request was submitted to Northumbrian Water Ltd. A response is currently awaited.

2.3. Redcar & Cleveland Borough Council

An enquiry was submitted to Redcar & Cleveland Borough Council, the LLFA. A copy of the response received is included in **Appendix A** and summarised below:

- The Ordinary Watercourse located approximately 120m to the south-west of the Site has historical flooding issues. Flood water discharges onto Tees Dock road area and causes road closures frequently during heavy and/or prolonged rainfall. The LLFA have had to manage flooding from this location in the past.
- The LLFA requires the Flood Risk Assessment & Drainage Strategy to be compliant with *Redcar and Cleveland Borough Council Local Plan (adopted May 218)* Planning Policy SD 7.



3. Site Description

3.1. Location

The Site is located within the former Redcar Steelworks, in the Lackenby area, approximately 2km south-west of Redcar. The Site is surrounded by now redundant industrial buildings and infrastructure which formed part of the former steelworks site (BOS & Concast). The wider site is now in the ownership of South Tees Development Corporation. Trunk Road and Tees Dock Road run approximately 100m to the east and 200m to the south of the Site respectively. A site location plan is shown in Figure 3-1.



Figure 3-1 Location plan (Not to scale)

3.2. Topography

The Site has a total area of approximately 4.50ha. The topographical survey of the Site is shown on drawing number 2383_JSH024 in **Appendix B**.

The Site's northern area is currently occupied by several stockpiles of industrial materials from former steel works operations, which have been abandoned. Ground levels within the Site, with the exception of the stockpiles, vary between approximately 9.5m AOD to 10.0m AOD. The surrounding industrial area is almost completely flat, with ground levels similar to the Site levels.

3.3. Land Use

3.3.1. Historic

According to old Ordnance Survey maps, the Site and the surrounding area was undeveloped agricultural land until the late 19th century. From 1895, areas surrounding the Site became progressively more developed and industrialised. Maps from the 1960s, show the Site developed as part of the Redcar Steelworks, with industrial



buildings present in the northern area. Maps from 2017 do not show these buildings with the area now occupied by stockpiles of abandoned industrial materials.

3.3.2. Current

The Site is currently a previously developed brownfield site. The northern area surface comprises of compacted soil and granular materials. There are also base slabs associated with previously demolished buildings. This northern area is currently occupied by several stockpiles of abandoned industrial materials. The southern part of the Site is vegetated with grass and small bushes.

The surrounding area comprises of decommissioned industrial buildings and infrastructure which were part of the former Redcar Steelworks.

3.4. Ground Conditions

The content of this section has been informed by a Geotechnical Risk Assessment Report prepared by Arcadis (reference: AUK-XX-XX-RP-GE-0001-01-SSI3_GI_GRA; date: November 2018) together with information from a number of on-line public domain data sources.

3.4.1. Soils

According to Soilscapes³, the soils on the Site are described as *slowly permeable seasonally wet slightly acid but base-rich loamy and clayey soils* with impeded drainage.

3.4.2. Made Ground

Made Ground is known to be on Site associated with the historical use of the site and the various stockpiles of industrial material.

The Geotechnical Risk Assessment Report has identified Made Ground to extend to depths of 4m or greater. The Made Ground is described to comprise slag deposits with fragments of slag ranging from gravel to cobble and occasionally boulder size. Other Made Ground materials were also identified including refractory bricks, demolition wastes and cohesive made ground.

3.4.3. Superficial Deposits

The Geotechnical Risk Assessment Report has identified that the Site is underlain by a sequence of superficial deposits comprising Glaciolacustrine Deposits and Glacial Till.

Glaciolacustrine Deposits were found to include a firm laminated clay, with silt along the laminations. Laboratory testing indicated the clay to be of medium or high plasticity.

Glacial Till predominantly comprising firm becoming stiff slightly sandy slightly gravelly clay, with boulders was recorded in some boreholes. Glacial Till can comprise a complex and variable sequence of soils which may also include sands and gravels, large boulders etc. Ground conditions may vary rapidly both laterally and vertically. At some locations, the Glaciolacustrine Deposits were found to be present between an upper and lower Glacial Till layer.

3.4.4. Bedrock

The Geotechnical Risk Assessment Report has identified the bedrock beneath the Site to be Redcar Mudstone and Mercia Mudstone formations, with the latter containing a significant proportion of gypsum.

3.4.5. Contamination

Based on the historic industrial uses of the Site, the ground is likely to be contaminated. Further information related the contamination present is presented in the Geotechnical Risk Assessment Report.

³ Soilscapes, <u>www.landis.org.uk/soilscapes/</u>



3.5. Water Environment

3.5.1. Drainage

3.5.1.1. Private Drainage

Drainage plans showing surface and foul water sewers associated with the former steel works site were obtained; however, no distinction is made between private and public sewers. Drainage plans are provided in **Appendix B**. These show that there are no sewers located within the Site. There are surface water sewers, believed to be private, nearby the Site's western, northern and eastern boundary.

Measures will be taken as part of the proposed works to ensure that none of those existing sewers are adversely impacted.

3.5.1.2. Public Sewerage

Drainage plans obtained (provided in **Appendix B**) make no distinction between private and public sewers. These show that there is a foul water sewer, believed to be publicly owned, running along Tees Dock Road, to the southwest of the Site. This sewer crosses Tees Dock Road and flows in south-westerly direction.

3.5.1.3. Land Drainage

There is no evidence available of any land drainage systems being present within the Site. If any land drainage is encountered during construction, it will be reconnected and/or diverted to ensure continuity of drainage post-development.

3.5.2. Watercourses

There is an unnamed Ordinary Watercourse located approximately 120m to the south-west of the Site. This watercourse flows in a generally northerly direction, entering a culvert running underneath the former Redcar Steelworks site.

The Knitting Wife Beck and Kinkerdale Beck, designated Ordinary Watercourses, are located approximately 500m to the south-west and 500m to the east of the Site respectively. These watercourse merge approximately 450m south-east of the Site before flowing in a broadly northerly direction into a culvert that runs underneath the A1085 and the former steelworks.

The estuary of the River Tees, designated a Main River, is located approximately 2.5km to the north-west of the Site.

3.5.3. Waterbodies

There are no waterbodies located within the Site.

There is a small ground depression and a pond located close to the southern boundary and approximately 50m to the south-west of the Site respectively.

The North Sea coast is located approximately 5km to the north of the Site.

3.5.4. Groundwater

According to Environment Agency mapping, the Site is not located within any groundwater Source Protection Zones. There are no superficial deposits underlying the Site. The bedrock underlying the Site is classified as a *Secondary (undifferentiated) Unproductive* aquifer.

The Geotechnical Risk Assessment Report has identified groundwater as being present at depths between 1.0m and 2.0m below original ground level.



4. Proposed Development

4.1. Description

The Proposed Development comprises a compacted steel fines surface to form soil treatment area, an associated drainage system and a water treatment plant.

The proposed indicative development layout (drawing reference: TSWK-STDC-LAC-ZZ-DR-C-0012) is included in **Appendix B**.

4.2. Sequential Test

According to the Environment Agency Flood Map, shown in Figure 4-1, the Site is located wholly within Flood Zone 1 (low risk; <0.1% annual exceedance probability (AEP)).

According to the Planning Practice Guidance², Table 2, the Proposed Development is classified as *More Vulnerable* as it is used as a waste management facility for hazardous waste. Planning Practice Guidance, Table 3 shows that *More Vulnerable* development within *Flood Zone 1* is compatible hence the Proposed Development is deemed to pass the Sequential Test.



Source: Environment Agency

Figure 4-1 Environment Agency Flood Map

5. Flood Risk Assessment

5.1. Flooding History

Consultation with the EA has established that they have no records of flooding at the site. This does not necessarily mean that the site has never flooded, only that the EA do not currently have records of flooding in this area.

Consultation with Redcar & Cleveland Borough Council confirmed historical flooding occurring to the south of the Site associated with the Ordinary Watercourse located approximately 120m to the south-west of the Site, which causes Tees Dock road closures during heavy and/or prolonged rainfall.

5.2. Identification of Flooding Sources

Planning Practice Guidance² requires that the risk of flooding from the following sources be considered:

- Fluvial (river) The Environment Agency Flood Map shows the Site to be located within Flood Zone 1 (low risk; <0.1% AEP); although, as described in section 3.5.2, there are three small watercourses flowing to the south-west and south-east of the Site. In the event of a flood associated with one of these watercourses, water is unlikely to be able to reach the Site due to topographical features and infrastructure such as roads, railways and pipelines. Therefore, the risk of fluvial flooding is considered to be low and does not require further assessment.
- **Coastal, tidal and estuarine** As described in section 3.5.2 and 3.5.3, the estuary of the River Tees and the coast facing the North Sea are located approximately 2.5km to the north-west and 5km to the north of the Site respectively. The Environment Agency Flood Map does not indicate that the Site is at risk from tidal flooding. On this basis, the risk associated with tidal flooding is considered to be low and no further assessment is necessary.
- **Surface water** The Environment Agency Surface Water Flood Map, included in Figure 5-1, shows minor areas within the site boundary, that may be affected by surface water flooding. Anecdotal evidence from the Site indicates that flooding is not known to have occurred in the past; however surface water is known to build up on the adjacent roads during periods of heavy rainfall. As a consequence, further consideration of surface water flood risk is required.
- **Groundwater** There have been no reports of groundwater flooding within or in the general vicinity of the Site. As described in section 3.5.4, groundwater levels has been identified at depths between 1.0m and 2.0m; however, the flat topography of the Site and surrounding areas is flat and the underlying soils and geology are of low permeability so the risk of groundwater emergence is low. On this basis, no further consideration of groundwater flooding is required.
- Sewers According to information from the Northumbrian Water DG5 Register included in the Strategic Flood Risk Assessment, there are no recorded sewer flooding incidents in the vicinity of the Site. Therefore, the risk of sewer flooding is considered low and further assessment is not required.
- **Artificial sources** There are no impounded water bodies at an elevation higher than the Site; therefore, the risk associated with this source is negligible and does not require further assessment.





Source: Environment Agency

Figure 5-1 Environment Agency Surface Water Flood Map

On the basis of the above, the risk assessment section below establishes the risks associated with surface water flooding only. The risks from fluvial, tidal, groundwater, sewers and artificial sources are considered to be low and hence do not require assessment.

5.3. Risk Assessment

5.3.1. Surface Water

The Environment Agency Surface Water Flood Map, shown in Figure 5-1, shows that the majority of the Site is at a very low risk (<0.1% AEP) of surface water flooding.

There are small areas identified as being at medium (1%-3.3% AEP) and low (0.1%-1% AEP) risk of surface water flooding. These are primarily associated with minor variations in ground levels. Due to the site being almost flat, surface water will tend to accumulate in any depressions rather than flow away. There are no surface water flow paths running through the Site.

The variations in ground levels will be removed as a result of the proposed ground reprofiling for the Proposed Development hence there is likely to be a reduction in the risk of water accumulating.

The reprofiling operations will not change or block existing flow paths hence there will be no adverse change in surface water flood risk within or beyond the Site. As such the risk of surface water flooding on the Site or surrounding areas will not be adversely affected by the development proposals.

5.4. Flood Risk Management

The proposed development will incorporate the following flood risk management measures to mitigate the risks identified above:

• The soil treatment area is bounded in the eastern, southern and western edges by a 600mm high bund. The northern edge is approximately 1m higher than the adjacent ground level and the soil treatment area slopes in a southerly direction. These measures reduce the risk of surface water flows from the surrounding area entering the Proposed Development. Additionally, run-off generated within the Proposed Development is contained rather than allowing it flow onto the surrounding ground surface.



• The Proposed Development will incorporate a positive surface water drainage system, described further in section 6, that will intercept run-off from the soil treatment area.

5.5. Residual Risks

Residual risks are those risks that remain once the flood risk management measures described above have been implemented. These are typically associated with extreme events that overwhelm drainage systems and exceed the parameters used to design any mitigation measures.

The primary residual risk that will affect this development is a rainfall event (>20% AEP) that exceeds the capacity of the proposed surface water drainage system to both intercept and convey flows. During such an event, water that is unable to enter the formal drainage system of the slab will accumulate at the southern end of the soil treatment area and, in extreme cases, may overtop the 600mm high bund and flow onto the surrounding ground surface.

The flood risk management measures described in Section 5.4 will aid in mitigating the consequences of such an event.



6. Surface Water Drainage Strategy

6.1. Existing Drainage Regime

Since the demolition of the former steel works, run-off from the Site primarily flows over the ground surface, dispersing over a large area until it is intercepted by a watercourse or other drainage feature, or infiltrates into the ground. It is possible that some run-off is intercepted by parts of the private drainage infrastructure systems associated with the former steel works; however, the extents of this are unknown.

6.2. Proposed Outfall

Surface water run-off from the Proposed Development will be discharged into a local public foul water sewer located along Tees Dock Road to the south-west of the Site. Prior to discharge, all flows will be passed through a water treatment plant to remove pollutants originating from soil that is being processed.

As described in section 3.4.5, the ground beneath the Site is likely to be highly contaminated; therefore, infiltration as a means of surface water disposal is not considered viable due to the risk of mobilising contaminants.

6.3. Maximum Permitted Discharge Rate

The maximum discharge rate from the Proposed Development into the public surface water sewer will be limited to 5l/s. This flow rate has been agreed with Northumbrian Water by the designers of the water treatment plant. The discharge rate will be controlled using the pumps which feed the water treatment plant that have a peak flow capacity of 5l/s.

6.4. Integration of SuDS

The nature of the Proposed Development is such that SuDS are not considered viable for inclusion. The proposals include flow storage to balance flow rates prior to treatment and subsequent discharge from the Site. In addition, all run-off is to be treated in a water treatment plant. Due to site conditions, these features will be heavily engineered rather than relying on natural features and processes.

6.5. Proposed Strategy

The proposed surface water drainage strategy is illustrated on drawing number TSWK-STDC-LAC-ZZ-DR-C-0014; a copy is included in **Appendix B**.

Due to the temporary nature of the Proposed Development, the drainage infrastructure has been designed to accommodate a 20% AEP rainfall event under normal free flow conditions. No climate change allowance has been included within the design. The soil treatment hospital is anticipated to be required for a period of up to 5-years. The probability of a 20% AEP rainfall event occurring during the lifespan of the facility is 67.2%. Details of the consequences of a rainfall event exceeding the 20% AEP event occurring are provided later in this section.

Run-off from the Proposed Development will drain into a storage feature before being transferred into the proposed water treatment plant and subsequently discharged from the Site. Run-off from the proposed soil treatment area will drain into a concrete channel running along the full length of the southern edge of the area. The peak run-off flow rate from the soil treatment area during the 20% AEP rainfall event has been calculated to be 189l/s, based on a rainfall intensity of 57.0mm/hr. The channel has been designed with a 1 in 250 longitudinal fall. The size of the channel has been designed to facilitate easy removal of accumulated silt.

The proposed channel will include a total of five outlets. Each outlet has been calculated to have a capacity of 52l/s. Provided that all the outlets are operational, the maximum flow rate to be conveyed by each will be 37.8l/s. The extra capacity within each outlet means that the system is capable of operating with some restrictions caused by potential build-up of silt and it is possible for one outlet to fail completely without adversely affecting the performance of the system. This resilience will enable the system to function within a high sediment load environment and also be capable of withstanding some rainfall events that exceed its design parameters.

Flow is conveyed from the proposed outlets to the storage tank via a 450mm diameter carrier pipe. The storage tank is proposed to be an open structure, either a lined basin or an open tank formed of precast concrete sections. Pumps will be used to transfer water from the storage to the proposed treatment plant; therefore, the base level of the tank is not constrained by downstream features. The storage volume required to



accommodate the 20% AEP rainfall event has been calculated using MicroDrainage Source Control to be 240m³. The calculations are included in **Appendix C**. The plan dimensions of the storage tank can be adjusted to suit the available space with the depth set to achieve the required volume. The following must be considered when determining the tank depth and levels:

- A freeboard of at least 0.2m must be provided between the maximum water level and the top of the tank.
- The maximum water level in the tank must not exceed 8.9m AOD (lowest level of the proposed channel along the southern edge of the soil treatment area).

The pumping arrangements from the storage tank into the proposed treatment plant are to be designed by others.

While the system has been designed to accommodate up to and including the 20% AEP rainfall event, it is able to manage more extreme rainfall events by using capacity normally contained within freeboard zones. The proposed soil treatment area is surrounded by a 600mm high bund which will retain water within the area if it is unable to drain via the channel and associated outlets. If the freeboard within the storage tank is used, this will enable water to accumulate within the soil treatment area to a depth of 0.2m. This will provide a further 142m³ of storage which is sufficient to accommodate the 5.5% AEP rainfall event.

In the event of more extreme rainfall, water will start to spill from the storage tank and potentially directly from the soil treatment area. Under these circumstances, the water will tend to flow in a south-easterly and south-westerly direction towards existing watercourses. There are no buildings or other critical facilities within this area that would be adversely affected.

6.6. Adoption & Maintenance

It is anticipated that the proposed surface water drainage system will be privately owned by South Tees Development Corporation and maintained on their behalf by a contractor.



7. Conclusions & Recommendations

7.1. Conclusions

The Site is located within Flood Zone 1 (low risk; <0.1% AEP) according to the Environment Agency Flood Map. There are three small watercourses in the vicinity of the Site. In the event of a flood associated with one of these watercourses, flood water is unlikely to be able to reach the Site due to topographical features and infrastructure such as roads, railways and pipelines. On this basis, the risk of fluvial flooding is considered to be low.

Environment Agency mapping shows small areas within the site boundary that may be affected by surface water flooding. These are primarily associated with minor variations in ground levels that result in depressions that could retain water. These variations will be removed as a result of the proposed ground reprofiling for the Proposed Development hence there is likely to be a reduction in the risk of water accumulating. The reprofiling operations will not change or block existing flow paths hence there will be no adverse change in surface water flood risk within or beyond the Site.

The risks from tidal, groundwater, sewers and artificial sources are considered to be negligible or low.

The Proposed Development will include the following flood risk management measures:

- A 600mm high bund bounding the soil treatment area's eastern, southern and western edges.
- The northern edge of the soil treatment area is approximately 1m higher than the adjacent ground level with the soil treatment area sloping in a southerly direction.
- A positive surface water drainage system.

The primary residual risk that will affect this development is a rainfall event (>20% AEP) that exceeds the capacity of the proposed surface water drainage system to both intercept and convey flows. During such an event, water that is unable to enter the formal drainage system will accumulate at the southern end of the soil treatment area and, in extreme cases, may overtop the 600mm high bund and flow onto the surrounding ground surface.

The proposed surface water drainage system will discharge surface water run-off from the Proposed Development into a local public foul water sewer located along Tees Dock Road to the south-west of the Site. Prior to discharge, all flows will be passed through a water treatment plant to remove pollutants originating from soil that is being processed. The discharge rate from the Proposed Development into the public surface water sewer will be limited to 5l/s.

The nature of the Proposed Development is such that SuDS are not considered viable for inclusion.

Due to the temporary nature of the Proposed Development, the drainage infrastructure has been designed to accommodate a 20% AEP rainfall event under normal free flow conditions. No climate change allowance has been included within the design.

Run-off from the Proposed Development will drain into a storage feature before being transferred into the proposed water treatment plant and subsequently discharged from the Site. The storage tank is proposed to be an open structure, either a lined basin or an open tank formed of precast concrete sections. Pumps will be used to transfer water from the storage to the proposed treatment plant. The storage volume required to accommodate the 20% AEP rainfall event has been calculated using MicroDrainage Source Control to be 240m³. A freeboard of at least 0.2m must be provided between the maximum water level and the top of the tank.

While the system has been designed to accommodate up to and including the 20% AEP rainfall event, it is able to manage more extreme rainfall events by using capacity normally contained within freeboard zones. The proposed soil treatment area is surrounded by a 600mm high bund which will retain water within the area if it is unable to drain via the channel and associated outlets. If the freeboard within the storage tank is used, this will enable water to accumulate on the slab to a depth of 0.2m. This will provide a further 142m³ of storage which enables the system to accommodate up to and including the 5.5% AEP rainfall event.

In the event of more extreme rainfall, water will start to spill from the storage tank and potentially directly from the soil treatment area. Under these circumstances, the water will tend to flow in a south-easterly and south-westerly direction towards existing watercourses. There are no buildings or other critical facilities within this area that would be adversely affected.

The surface water drainage system is anticipated to be privately owned by South Tees Development Corporation and maintained on their behalf by a contractor.



7.2. Recommendations

This Flood Risk Assessment is suitable for submission in support of a full planning application for the Proposed Development.

The design of the Proposed Development and its drainage systems must comply with the principles and parameters defined in this document.

Appendices

TSWK-STDC-LAC-RPT-C-0001 | 1.0 | 12 May 2021 Atkins | TSWK-STDC-LAC-RPT-C-0001-1 Flood Risk Assessment.docx



Appendix A. Correspondence

Lazzarin, Filippo

From:	Northeast Newcastle, Customer Contact <northeast-newcastle@environment-< th=""></northeast-newcastle@environment-<>
	agency.gov.uk>
Sent:	05 March 2021 09:47
То:	Lazzarin, Filippo
Subject:	Our ref: 206840 - FW: 210224/DR08 Enquiry regarding Help & advice for FRA -
	(Redcar, TS6 7RT)

Our Ref: 206840

DearFilippo,

Enquiry regarding FRA - Redcar, TS6 7RT

Thank you for your enquiry which was received on 22 February 2021.

We can confirm that your site of interest is within Flood Zone 1. Following examination of our records of historic flooding, we have no record of flooding in the area. This does not necessarily mean that the area of the property / site has never flooded, only that we do not currently have records of flooding in this area.

The Lead Local Flood Authority now agree drainage discharge rates. Please contact the LLFA to discuss this matter with them.

The Environment Agency is the relevant risk management authority for flood risk on 'main rivers'. Local Authorities now take the lead for local flood risk, including 'ordinary watercourses', surface water and ground water flooding. We recommend that you contact the Lead Local Flood Authority for further information. Regarding flood risk from sewers please contact Northumbrian Water Group.

For general advice about assessing flood risk when completing planning applications, and in particular how to complete a flood risk assessment (FRA) as part of a planning application go to <u>https://www.gov.uk/guidance/flood-risk-assessment-for-planning-applications</u>

Our Sustainable Places Team can give more detailed advice although there is a charge for this. Here is the link to the standard terms and conditions that apply to our charged planning advice service https://www.gov.uk/government/publications/planning-advice-environment-agency-standard-terms-and-conditions. The standard charge is £100 per hour.

We hope we have answered your query. Please see the following link for details of permitted use - <u>http://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/</u>

We respond to requests for recorded information that we hold under the Freedom of Information Act 2000 (FOIA) and the associated Environmental Information Regulations 2004 (EIR).

If you are not satisfied with our response to your request for information you can contact us within 2 calendar months to ask for our decision to be reviewed.

We now have over 100 datasets available as Open Data. Open Data allows access to our data free of charge and free of restriction, even for commercial use under an Open Government Licence. You can find out about the data we have available our new page on <u>Gov.uk https://www.gov.uk/environmental-data</u>

Please don't hesitate to contact me if you have any further queries.

Kind regards,

Carole Anne Pollock,

North East Customers and Engagement Team Environment Agency | Tyneside House, Skinnerburn Road, Newcastle, NE4 7AR

Normal working hours: Tue-Fri 07:00-15:00

M: 07584526496 DD: 02077 142957

For all Freedom of Information related enquiries please send your email to <u>northeast-newcastle@environment-</u> agency.gov.uk

Environment Agency staff are working from home due to the Coronavirus (COVID-19) pandemic. All staff can be contacted via e-mail or telephone as usual. Please accept our apologies in advance for any delays in our service during this time, which we are minimising as much as possible.





From: Lazzarin, Filippo [mailto:Filippo.Lazzarin@atkinsglobal.com]
Sent: 22 February 2021 17:05
To: Enquiries, Unit <enquiries@environment-agency.gov.uk>
Cc: Birkenshaw, Paul <Paul.Birkenshaw@atkinsglobal.com>
Subject: Enquiry regarding Help & advice for FRA - (Redcar, TS6 7RT)

Good Afternoon,

We are contacting you with reference to a proposed temporary soil treatment facility plant (lasting approximately five years) in Redcar, North Yorkshire. Please see site location details below and site location plan attached.

Site Location: Former Redcar Steelworks site, Redcar, North Yorkshire, TS6 7RT

NGR coordinates: 455489 ; 521303

We are preparing a Flood Risk Assessment to support a planning application and we would be grateful if you could confirm the following:

• The site lies within Flood Zone 1. Please could you confirm this and advise whether there are any records of flooding from any source in the vicinity of the site.

• Are you aware of any specific flood risk and/or drainage issues that we should take into account within the Flood Risk Assessment and drainage strategy for this site?

Please contact me if you require any clarification about this enquiry.

Kind Regards

Filippo Lazzarin *MEng* Assistant Civil Engineer, Infrastructure UK & Europe Engineering, Design & Project Management

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Lazzarin, Filippo

Lyndsey Hall <lyndsey.hall@redcar-cleveland.gov.uk></lyndsey.hall@redcar-cleveland.gov.uk>
07 May 2021 13:41
Lazzarin, Filippo
David Pedlow; Nigel Hill
RE: Development Enquiry LLFA - (Redcar, TS6 7RT)

Good afternoon Filippo,

Apologies for the delay in responding, unfortunately I have been on extended leave. Please see below;

Boundary beck which runs just south of the right boundary line (within the blue line area) has historical flooding issues. Flood water discharges onto Tees Dock road area and causes road closures frequently during heavy and/or prolonged rainfall.

I would advise a discussion with Teesworks and British steel, they may have more detail on this flooding issue as the site is in their private ownership. The LLFA have had to manage flooding from this location recently.

With regards to a planning submission please ensure the FRA & Drainage Strategy is compliant with Redcar and Cleveland Borough Council Planning Policy SD7 of the Local Plan (adopted May 218)

If you require further assistance please contact Nigel Hill who is happy to discuss further in more detail.

Kind regards

Lyndsey

Lyndsey Hall BA (Hons) PGDip FCRM Engineer Engineering Services Redcar & Cleveland Borough Council

Direct Line: 01287 612343 Mobile: 07557 481108 Email: Lyndsey.hall@redcar-cleveland.gov.uk

Corporate Directorate for Growth, Enterprise and Environment Redcar & Cleveland House Kirkleatham Street Redcar Yorkshire TS10 1RT



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"A FLOURISHIN	OUR N IG FUTURE FO OUR N	/ISION RGED FROM A /ALUES	PROUD PA
KEEPING COMMUNITIES AT OUR HEART	BOLD AND AMBITIOUS	CARING AND RESPECTFUL	DELIVERING OUR BEST

From: Lazzarin, Filippo
Sent: 22 February 2021 17:06
To: contactus@redcar-cleveland.gov.uk
Cc: Birkenshaw, Paul <<u>Paul.Birkenshaw@atkinsglobal.com</u>>
Subject: Development Enquiry LLFA - (Redcar, TS6 7RT)

Good Afternoon,

We are contacting you, as the LLFA, with reference to a proposed temporary soil treatment facility plant (lasting approximately 5 years) which our client is intending to submit a planning for in Redcar, North Yorkshire. Please see site location details below and site location plan attached.

Site Location: Former Redcar Steelworks site, Redcar, North Yorkshire, TS6 7RT

NGR coordinates: 455489 ; 521303

The site is currently a brownfield site, located within the Former Redcar Steelworks in the industrial area generally known as 'South Tees'. The site is accessed via the Lackenby Gate Entrance along Trunk Road.

As part of the drainage strategy, we are looking to treat surface water run-off from the site, before discharging it into the local surface water network.

Could you please advise on site specific requirements and historic flooding?

We look forward to hearing from you.

Kind Regards, Filippo Lazzarin *MEng* Assistant Civil Engineer, Infrastructure UK & Europe Engineering, Design & Project Management



~
-

Atkins The Axis, 10 Holliday Street, Birmingham, B1 1TF

Company	xxxx

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Redcar & Cleveland Borough Council, Redcar & Cleveland House, Kirkleatham Street, Redcar, TS10 1RT, Tel: 01642 774 774, Website: <u>www.redcar-cleveland.gov.uk</u>



Appendix B. Drawings







WORKS LACKENBY	plant GEI
SECTION OF PLANT DRAINAGE	L
SUB-SECTION OF PLANT OWNERSHIP BOUNDA	RY
PEDS CODE (7/2/2)	INDEX C

		<u>NOT</u> 1.	ES REFER SKETCH CROSSI	TO DRA I TO DE ES BOUN	WING INF_08_ TERMINE OWN NDARY	_057_06 FO ERSHIP WHE	R OWNERSHIP N DRAIN	
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268 - - -					SURFAC	e wate	r drain	
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	08_057							
22007	VING INF		K	<u>(EY</u> F	<u>Plan</u>			
_ ,	SEE DRAV							
	H-LINE							
::=.	MATC							
MH 554								
NDH			B	OWNERSH ISSUED F	IP BOUNDARY RE	EMOVED	DPK AF 05.3.09 05.3.09 DPK AF 24.2.09 24.2.09	
			Rev A	Description BK	on Consultar	nts Ltd.	Drawn Checked	
IH 557			1st Stee Rec TS1	Floor el House lcar 10 5QW				
			Tel e-m Drawn D.KE	ail: offic	05556 Fax ceabkconsultant Date 24/02/09	ts@btconnect. Checked A.FROST	48 .com Date 24/02/09	
			Client	Cor	Steel Redc	House ar 50W		
			Projec	Teess TEES DRAINA	ide Cast Pro	GATION WC	RKS	
MH 10C			Title	DRAINA	GE OWNERS	SHIP DRAW	/ING	
				SHEET	ļ			
ERAL			Scale 1:1	000		Client Nr.	9119 A	
DE)						_, с н авк nr. INF_08	_057_14B	







OFFSITE OWNER 1382 TCP OFFSITE OWNER WHERE THE SYSTEM LIES WITHIN LAND LEASED. THE SYSTEM REMAINS THE RESPONSIBILITY OF THE LAND OWNER.

WORKS LACKENBY	GENER
section of plant DRAINAGE	1
SUB-SECTION OF PLANT OWNERSHIP BOUNDA	RY
PEDS CODE (7/2/2)	INDEX CODE
	SM/12

		7
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REFEF INF_08_0 INF_08_0 INF_08_0 INF_08_0	RENCE DRAWINGS 057_06- FULL SITE OWNERSHIP DRAWING 057_14- SHEET 1 OF 5 057_16- SHEET 3 OF 5 057_17- SHEET 4 OF 5 057_18- SHEET 5 OF 5	
KEY		
	TCP OWNED	
	CORUS OWNED	
	BOS PLANT (TCP OWNED)	
	BEAM MILL (Corus owned)	
	COIL PLATE MILL	
	CORUS OWNED LEASED	
	FOUL WATER DRAIN SURFACE WATER DRAIN -	
	KEY PLAN	
A	ISSUED FOR INFORMATION DPK AF	
Rev	24.2.0924.2.09DescriptionDrawnChecked	
	ABK Consultants Ltd.	
1 S	st Floor teel House edcar	
T 1	S10 5QW el. 01642 405556 Fax. 01642 404648	
e	-mail: officeabkconsultants@btconnect.com	
D.	KELLY 24/02/09 A.FROST 24/02/09	



AO





		BOUNDARY	MANH	OLES
UPSTREAM		DOWNSTREAM		DRAIN PIPE OWNER BETWEEN MANHOLES
MANHOLE	OWNER	MANHOLE	OWNER	
708	CORUS	KINGFISHER POND	TCP	CORUS
CH3	TCP	CH4	CORUS	ТСР
1329	TCP	1325	CORUS	TCP
79	CORUS	59	TCP	CORUS

			······································	·····	
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		<u>KEY</u>			
_			TCP OWNE	D	
- /			CORUS OW	NED	
b r			BOS PLANT (TCP OWNE	ED)	
<u>u</u>			BEAM MILL (corus ov	VNED)	
			coil plate	E MILL	
			CORUS OW TO TCP	NED LEASED	
,		<u> </u>	FOUL W SURFAC	VATER DRAIN E WATER DRA	41N
	MATCH-LINE SEE DRAWING INF_08_057_17		KEY PLAN		
		B A Rev A 1st Stee Rec TS1	OWNERSHIP BOUNDARY R ISSUED FOR INFORMATION Description BK Consultar Floor el House icar 10 5QW	EMOVED DPK 05.3.09 04 DPK 24.2.09 24 Drawn CH nts Ltd.	AF 5.3.09 AF 4.2.09 hecked
		Drawn D.KE	ail: officeabkconsultan	ts@btconnect.com Checked Date A.FROST 24/C	2/09
		Project	COTUS Steel Redc COTUS TS10 Teesside Cast Pro	House ar 5QW oducts S	
		Title	DRAINAGE INVEST	GATION WORKS	
			SHEET 3		
ER	AL	Scale 1:1	000	Client Nr. A L/G 119121	
)DE	·			abk nr. INF_08_057_10	6B







Appendix C. Calculations

Atkins Limited		Page 1
Woodcote Grove	STDC Soil Hospital	
Epsom	Surface water drainage	
Surrey KT18 5BW	Design condition	Micro
Date 27/04/2021	Designed by PJB	Dcainago
File Storage tank.SRCX	Checked by FL	Diamage
Micro Drainage	Source Control 2019.1	•

Summary of Results for 5 year Return Period

Half Drain Time : 405 minutes.

	Stor	rm ht.	Max Level	Max Depth	Max Infiltration	Max Control	Max Σ Outflow	Max Volume	Stat	tus
			(m)	(m)	(1/s)	(1/s)	(1/s)	(m ³)		
15	min	Summer	8.045	0.545	0.0	5.0	5.0	92.7		ΟK
30	min	Summer	8.205	0.705	0.0	5.0	5.0	119.8		ΟK
60	min	Summer	8.365	0.865	0.0	5.0	5.0	147.1		ΟK
120	min	Summer	8.547	1.047	0.0	5.0	5.0	178.1		ΟK
180	min	Summer	8.638	1.138	0.0	5.0	5.0	193.5		ΟK
240	min	Summer	8.682	1.182	0.0	5.0	5.0	200.9		ΟK
360	min	Summer	8.710	1.210	0.0	5.0	5.0	205.8		ΟK
480	min	Summer	8.708	1.208	0.0	5.0	5.0	205.3		ΟK
600	min	Summer	8.689	1.189	0.0	5.0	5.0	202.1		ΟK
720	min	Summer	8.657	1.157	0.0	5.0	5.0	196.8		ΟK
960	min	Summer	8.580	1.080	0.0	5.0	5.0	183.6		ΟK
1440	min	Summer	8.478	0.978	0.0	5.0	5.0	166.3		ΟK
2160	min	Summer	8.339	0.839	0.0	5.0	5.0	142.6		ΟK
2880	min	Summer	8.214	0.714	0.0	5.0	5.0	121.3		ΟK
4320	min	Summer	8.010	0.510	0.0	5.0	5.0	86.6		ΟK
5760	min	Summer	7.854	0.354	0.0	5.0	5.0	60.1		ΟK
15	min	Winter	8.113	0.613	0.0	5.0	5.0	104.3		ΟK
30	min	Winter	8.291	0.791	0.0	5.0	5.0	134.4		ΟK
60	min	Winter	8.475	0.975	0.0	5.0	5.0	165.8		ΟK
120	min	Winter	8.687	1.187	0.0	5.0	5.0	201.8		ΟK
180	min	Winter	8.797	1.297	0.0	5.0	5.0	220.5		ΟK
240	min	Winter	8.861	1.361	0.0	5.0	5.0	231.4	Flood	Risk
360	min	Winter	8.912	1.412	0.0	5.0	5.0	240.0	Flood	Risk

Storm		Rain	Flooded	Discharge	Time-Peak	
	Event		(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
15	min	Summer	43.080	0.0	96.0	18
30	min	Summer	28.200	0.0	125.8	33
60	min	Summer	17.840	0.0	159.1	62
120	min	Summer	11.420	0.0	203.8	122
180	min	Summer	8.703	0.0	232.9	182
240	min	Summer	7.150	0.0	255.2	240
360	min	Summer	5.390	0.0	288.6	322
480	min	Summer	4.395	0.0	313.8	384
600	min	Summer	3.744	0.0	334.2	450
720	min	Summer	3.283	0.0	351.6	516
960	min	Summer	2.662	0.0	380.2	654
1440	min	Summer	1.977	0.0	423.4	924
2160	min	Summer	1.476	0.0	474.1	1324
2880	min	Summer	1.207	0.0	516.8	1728
4320	min	Summer	0.921	0.0	591.9	2464
5760	min	Summer	0.766	0.0	656.2	3168
15	min	Winter	43.080	0.0	107.6	18
30	min	Winter	28.200	0.0	140.9	33
60	min	Winter	17.840	0.0	178.2	62
120	min	Winter	11.420	0.0	228.3	120
180	min	Winter	8.703	0.0	261.0	178
240	min	Winter	7.150	0.0	285.9	234
360	min	Winter	5.390	0.0	323.3	344
		©	1982-20	19 Innc	ovyze	

Atkins Limited		Page 2
Woodcote Grove	STDC Soil Hospital	
Epsom	Surface water drainage	
Surrey KT18 5BW	Design condition	Micro
Date 27/04/2021	Designed by PJB	Dcainago
File Storage tank.SRCX	Checked by FL	Diamage
Micro Drainage	Source Control 2019.1	

Summary of Results for 5 year Return Period

	Storn Event	n E	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (1/s)	Max Σ Outflow (l/s)	Max Volume (m³)	Stat	us
480	min V	Winter	8.908	1.408	0.0	5.0	5.0	239.4	Flood	Risk
600	min V	Winter	8.885	1.385	0.0	5.0	5.0	235.5	Flood	Risk
720	min V	Winter	8.853	1.353	0.0	5.0	5.0	229.9	Flood	Risk
960	min V	Winter	8.763	1.263	0.0	5.0	5.0	214.8		ОК
1440	min V	Winter	8.582	1.082	0.0	5.0	5.0	183.9		ОК
2160	min V	Winter	8.352	0.852	0.0	5.0	5.0	144.8		ОК
2880	min V	Winter	8.148	0.648	0.0	5.0	5.0	110.2		ОК
4320	min V	Winter	7.833	0.333	0.0	5.0	5.0	56.6		ОК
5760	min V	Winter	7.650	0.150	0.0	5.0	5.0	25.0		ΟK

	Stor	cm	Rain	Flooded	Discharge	Time-Peak
	Ever	nt	(mm/hr)	Volume	Volume	(mins)
				(m³)	(m³)	
480	min	Winter	4 395	0 0	351 5	448
600	min	Winter	3.744	0.0	374.3	482
720	min	Winter	3.283	0.0	393.7	556
960	min	Winter	2.663	0.0	425.8	712
1440	min	Winter	1.977	0.0	474.3	1010
2160	min	Winter	1.476	0.0	531.0	1428
2880	min	Winter	1.207	0.0	578.9	1820
4320	min	Winter	0.921	0.0	663.0	2548
5760	min	Winter	0.766	0.0	734.9	632

Atkins Limited		Page 3
Woodcote Grove	STDC Soil Hospital	
Epsom	Surface water drainage	
Surrey KT18 5BW	Design condition	Micro
Date 27/04/2021	Designed by PJB	Dcainago
File Storage tank.SRCX	Checked by FL	Diamage
Micro Drainage	Source Control 2019.1	·

<u>Rainfall Details</u>

Rainfall Model						FEH
Return Period (years)						5
FEH Rainfall Version						2013
Site Location	GB	455477	521285	ΝZ	55477	21285
Data Type						Point
Summer Storms						Yes
Winter Storms						Yes
Cv (Summer)						0.750
Cv (Winter)						0.840
Shortest Storm (mins)						15
Longest Storm (mins)						5760
Climate Change %						+0

<u>Time Area Diagram</u>

Total Area (ha) 1.190

Time	(mins)	Area
From:	To:	(ha)

0 4 1.190

Atkins Limited		Page 4							
Woodcote Grove	STDC Soil Hospital								
Epsom	Surface water drainage								
Surrey KT18 5BW	Design condition	Micco							
Date 27/04/2021	Dcainago								
File Storage tank.SRCX	Checked by FL	Diamage							
Micro Drainage	Source Control 2019.1								
<u>Model Details</u> Storage is Online Cover Level (m) 9.100									
	<u>Complex Structure</u>								
	Tank or Pond								
	Tallk of Polid								
	Invert Level (m) 7.500								
Depth (m) Area (m ²) Depth (m) Area (m ²) Depth (m) Area (m ²)									
0.000 11	0.000 170.0 1.400 170.0 1.600 170.0								
	Tank or Pond								
	Invert Level (m) 8.900								
Depth	(m) Area (m²) Depth (m) Area (m²)								
0	.000 0.0 0.200 1420.0								
Level (Controlled Pump Outflow Control								
Invert Level (m) 7.50	0 Cut In Height (m) 0.150 Cut Out Height	(m) 0.000							
Depth (m) Outflow (1/s) Depth (m)	Outflow (1/s) Depth (m) Outflow (1/s) D	epth (m) Outflow (l/s)							
0.100 5.0000 0.900 0.200 5.0000 1.000 0.300 5.0000 1.100 0.400 5.0000 1.200 0.500 5.0000 1.300 0.600 5.0000 1.400 0.700 5.0000 1.500 0.800 5.0000 1.600	5.00001.7005.00005.00001.8005.00005.00001.9005.00005.00002.0005.00005.00002.1005.00005.00002.2005.00005.00002.3005.00005.00002.4005.0000	2.5005.00002.6005.00002.7005.00002.8005.00002.9005.00003.0005.0000							

Atkins Limited		Page 1
Woodcote Grove	STDC Soil Hospital	
Epsom	Surface water drainage	
Surrey KT18 5BW	Extreme event stress test	Micro
Date 27/04/2021	Designed by PJB	Dcainago
File Storage tank.SRCX	Checked by FL	Diamage
Micro Drainage	Source Control 2019.1	

Summary of Results for 18 year Return Period

Half Drain Time : 617 minutes.

	Storm Event		Max Level	Max Depth	Max Infiltration	Max Control	Σ	Max Outflow	Max Volume	Stat	cus
			(m)	(m)	(1/s)	(1/s)		(1/s)	(m³)		
15	min	Summer	8.326	0.826	0.0	5.0		5.0	140.4		ОК
30	min	Summer	8.583	1.083	0.0	5.0		5.0	184.1		ОК
60	min	Summer	8.843	1.343	0.0	5.0		5.0	228.3	Flood	Risk
120	min	Summer	8.999	1.499	0.0	5.0		5.0	266.5	Flood	Risk
180	min	Summer	9.031	1.531	0.0	5.0		5.0	286.7	Flood	Risk
240	min	Summer	9.044	1.544	0.0	5.0		5.0	298.2	Flood	Risk
360	min	Summer	9.056	1.556	0.0	5.0		5.0	309.2	Flood	Risk
480	min	Summer	9.057	1.557	0.0	5.0		5.0	310.4	Flood	Risk
600	min	Summer	9.055	1.555	0.0	5.0		5.0	308.0	Flood	Risk
720	min	Summer	9.051	1.551	0.0	5.0		5.0	304.5	Flood	Risk
960	min	Summer	9.039	1.539	0.0	5.0		5.0	293.8	Flood	Risk
1440	min	Summer	9.023	1.523	0.0	5.0		5.0	280.9	Flood	Risk
2160	min	Summer	9.002	1.502	0.0	5.0		5.0	267.9	Flood	Risk
2880	min	Summer	8.968	1.468	0.0	5.0		5.0	253.2	Flood	Risk
4320	min	Summer	8.796	1.296	0.0	5.0		5.0	220.3		ОК
5760	min	Summer	8.597	1.097	0.0	5.0		5.0	186.5		ОК
15	min	Winter	8.428	0.928	0.0	5.0		5.0	157.7		ОК
30	min	Winter	8.717	1.217	0.0	5.0		5.0	206.8		ОК
60	min	Winter	8.980	1.480	0.0	5.0		5.0	257.7	Flood	Risk
120	min	Winter	9.048	1.548	0.0	5.0		5.0	301.7	Flood	Risk
180	min	Winter	9.071	1.571	0.0	5.0		5.0	325.7	Flood	Risk
240	min	Winter	9.083	1.583	0.0	5.0		5.0	341.3	Flood	Risk
360	min	Winter	9.094	1.594	0.0	5.0		5.0	356.9	Flood	Risk

	Storm		Rain	Flooded	Discharge	Time-Peak	
	Event		(mm/hr)	Volume	Volume	(mins)	
				(m³)	(m³)		
15	min	Summer	64.616	0.0	144.1	19	
30	min	Summer	42.756	0.0	190.8	33	
60	min	Summer	27.159	0.0	242.4	64	
120	min	Summer	16.517	0.0	294.8	122	
180	min	Summer	12.320	0.0	329.9	182	
240	min	Summer	9.997	0.0	356.9	242	
360	min	Summer	7.441	0.0	398.5	360	
480	min	Summer	6.031	0.0	430.6	468	
600	min	Summer	5.128	0.0	457.7	518	
720	min	Summer	4.494	0.0	481.4	584	
960	min	Summer	3.659	0.0	522.6	712	
1440	min	Summer	2.754	0.0	589.9	982	
2160	min	Summer	2.097	0.0	673.9	1404	
2880	min	Summer	1.737	0.0	744.2	1816	
4320	min	Summer	1.338	0.0	859.5	2632	
5760	min	Summer	1.112	0.0	953.1	3400	
15	min	Winter	64.616	0.0	161.4	19	
30	min	Winter	42.756	0.0	213.7	33	
60	min	Winter	27.159	0.0	271.5	62	
120	min	Winter	16.517	0.0	330.2	120	
180	min	Winter	12.320	0.0	369.5	178	
240	min	Winter	9.997	0.0	399.7	236	
360	min	Winter	7.441	0.0	446.3	352	
		©	1982-20	19 Inno	ovyze		

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Woodcote Grove	STDC Soil Hospital	
Epsom	Surface water drainage	
Surrey KT18 5BW	Extreme event stress test	Micro
Date 27/04/2021	Designed by PJB	Dcainago
File Storage tank.SRCX	Checked by FL	Diamage
Micro Drainage	Source Control 2019.1	

Summary of Results for 18 year Return Period

	Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (l/s)	Max Σ Outflow (l/s)	Max Volume (m ³)	Status
480	min Wint	er 9.098	1.598	0.0	5.0	5.0	362.8	Flood Risk
600	min Wint	er 9.098	1.598	0.0	5.0	5.0	362.7	Flood Risk
720	min Wint	er 9.095	1.595	0.0	5.0	5.0	358.7	Flood Risk
960	min Wint	er 9.088	1.588	0.0	5.0	5.0	348.5	Flood Risk
1440	min Wint	er 9.070	1.570	0.0	5.0	5.0	325.6	Flood Risk
2160	min Wint	er 9.046	1.546	0.0	5.0	5.0	300.0	Flood Risk
2880	min Wint	er 9.009	1.509	0.0	5.0	5.0	271.8	Flood Risk
4320	min Wint	er 8.752	1.252	0.0	5.0	5.0	212.8	0 K
5760	min Wint	er 8.417	0.917	0.0	5.0	5.0	155.9	0 K

Storm Event		Rain (mm/hr)	Flooded Volume	Discharge Volume	Time-Peak (mins)
			(m³)	(m³)	
min	Winter	6.031	0.0	482.3	462
min	Winter	5.128	0.0	512.6	572
min	Winter	4.494	0.0	539.1	672
min	Winter	3.659	0.0	585.3	762
min	Winter	2.754	0.0	660.6	1070
min	Winter	2.097	0.0	754.7	1536
min	Winter	1.737	0.0	833.5	1964
min	Winter	1.338	0.0	962.6	2808
min	Winter	1.112	0.0	1067.5	3576
	stor Even min min min min min min min min	Storm Event min Winter min Winter min Winter min Winter min Winter min Winter min Winter min Winter	StormRain (mm/hr)Event6.031min Winter5.128min Winter4.494min Winter3.659min Winter2.754min Winter2.097min Winter1.737min Winter1.338min Winter1.112	StormRainFloodedEvent(mm/hr)Volume (m³)min Winter6.0310.0min Winter5.1280.0min Winter4.4940.0min Winter3.6590.0min Winter2.7540.0min Winter2.0970.0min Winter1.7370.0min Winter1.3380.0min Winter1.1120.0	Storm Rain Flooded Discharge Event (mm/hr) Volume Volume (m³) (m³) (m³) min Winter 6.031 0.0 482.3 min Winter 5.128 0.0 512.6 min Winter 4.494 0.0 539.1 min Winter 3.659 0.0 585.3 min Winter 2.097 0.0 660.6 min Winter 1.737 0.0 833.5 min Winter 1.338 0.0 962.6 min Winter 1.112 0.0 1067.5



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